

# **Technical Memorandum**

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Groundwater model simulations were conducted by Barr Engineering to estimate future water table conditions near Freeway Landfill after dewatering ceases at the Kraemer Quarry located directly south of the landfill. The anticipated rise in the water table is compared against the bottom of the waste that was identified in previous MPCA investigations to assess the potential for the waste in the landfill to come into contact with the predicted higher water table. This memorandum is a brief summary of the results. Further documentation and reporting are currently in process.

A refined, local scale, version of the Twin Cities Metropolitan Area Regional Groundwater Flow Model, Version 3.0 (Metropolitan Council, 2014) was used for the analysis and simulation of future conditions. A telescopic mesh refinement of the regional model was created. Five additional layers were added to better simulate flow conditions within the Prairie du Chien Group, the upper most bedrock at the landfill and the unit currently being quarried. Additional calibration of the model was conducted using data collected in January, 2015 at and near the Freeway Landfill.

After calibration, the model was used to simulate potential future conditions with varying pit-lake stages to estimate the water table elevation within the footprint of the waste at the Freeway Landfill. To address uncertainties in the model simulations, Latin hypercube sampling (Swiler and Wyss, 2004; Watermark Numerical Computing, 2012) was used to generate 1000 unique parameter sets, allowing parameters to vary over expected ranges. Model simulations were then conducted using these parameter sets and the results were compared to the calibration dataset. Parameter combinations that resulted in no more than a 5% increase in the calibration objective function (error of best-fit model to measured data) were deemed acceptable and carried forward for use in simulating potential future conditions. Parameter sets that resulted in more than a 5% increase in the calibration objective function were deemed unacceptable (i.e., poor model fit) and excluded from further analysis. A total of 298 unique parameter combinations, out of 1000 possible, were ultimately used for uncertainty analysis.

For each unique parameter set a series of steady-state simulations were conducted. First, pumping from Kraemer Quarry was reduced to include only pumping for the City of Burnsville supply. The average reported pumping from the quarry for Burnsville from 2010 to 2013 of 3.4 million gallons per day was

used; no pumping was included for quarry dewatering operations (8.4 MGD average for 2010-2013) since this scenario was intended to simulate conditions after the Quarry ceases operations. Second, a series of simulations were conducted where pumping rates from the Quarry were adjusted to achieve pit-lake stages between 205 meters and 213 meters (672.6 feet to 698.8 feet) in one meter increments. For each simulation, the simulated water table elevation was compared to the bottom of waste at the Freeway Landfill as measured by Gorman Surveying (2005). The results of these simulations are summarized on Figures 1 to 11 and in Tables 1 and 2. The range of results (minimum, average, and maximum) using all 298 unique parameter sets as defined above are shown. The waste saturation for the various scenarios is estimated as a percentage of the landfill footprint coming into contact with the groundwater (i.e., percentage of area, not percentage of volume).

### **Table 1. Results of simulations with pumping from Kraemer Quarry for Burnsville supply only, no dewatering for quarry operations.**





### **Table 2. Results of simulations maintaining pit-lake at specified stage.**

# **References**

- Gorman Surveying, Inc. 2005. Freeway Landfill subsurface exploration results, Job Number 05-032, Sheet 2 of 2.
- Metropolitan Council. 2014. Twin Cities Metropolitan Area Regional Groundwater Flow Model, Version 3.0. Prepared by Barr Engineering. Metropolitan Council: Saint Paul, MN.

Swiler, L.P. and Wyss, G.D. 2004. A User's Guide to Sandia's Latin Hypercube Sampling Software: LHS UNIX Library/Standalone Version. Sandia National Laboratories, Report SAND2004-2439.

Watermark Numerical Computing. 2012. PEST Utilities to complement Latin Hypercube Sampling Software developed by Sandia National Laboratories.

I hereby certify that this plan, document, or report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Geologist under the laws of the state of Minnesota.

Digitally signed by John C. Greer DN: cn=John C. Greer, o=Barr Engineering Co., ou, email=jgreer@barr.com, c=US Date: 2015.04.13 12:28:03 -05'00'

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April 13, 2015

Date



 Red horizontal line indicates the range in simulated pit-lake stage with pumping only for Burnsville supply Vertical orange lines indicate historical minimum, maximum, and average stage for the Minnesota RiverVertical green line indicates the lowest measured elevation for the bottom of waste in the Freeway Landfill SUMMARY OF SIMULATIONSOF FUTURE CONDITIONS



Minimum Saturated Thickness Above Bottom of Waste Standard Deviation of Water Table Elevation



Standard Deviation of Water Table Elevation

0.03 - 0.10

 $0.11 - 0.15$ 

0.16 - 0.20

0.21 - 0.25

(m)

 $\bullet$ 

 $\bullet$ 

 $\bullet$ 

Saturated Thickness Above Waste (m)

- Dry
- $\bullet$  $0.1 - 0.5$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0
- 
- 2.1 2.5
- > 2.5 m









# WASTE SATURATION BURNSVILLE PUMPING ONLY





Standard Deviation of Water Table Elevation

 $< 0.05$ 

0.06 - 0.10

0.11 - 0.15

0.16 - 0.20

(m)

 $\bullet$ 

 $\bullet$ 

 $\bullet$  $\bullet$ 

Saturated Thickness Above Waste (m)

- Dry
- $\bullet$  $0.1 - 0.5$
- $0.6 1.0$  $\bullet$
- $\bullet$  $1.1 - 1.5$
- 1.6 2.0
- 
- 2.1 2.5
- > 2.5 m











WASTE SATURATION PIT LAKE AT 205 METERS (672.6 FT)





(m)

 $\bullet$ 

 $\bullet$ 

 $< 0.05$ 

Saturated Thickness Above Bottom of Waste (m)

- Dry
- $\bullet$  $0.1 - 0.5$
- $\bullet$  $0.6 - 1.0$
- $1.1 1.5$  $\bullet$
- 1.6 2.0  $\bullet$
- 2.1 2.5
- > 2.5 m

Average Saturated Thickness Above Bottom of Waste Maximum Saturated Thickness Above Bottom of Waste









WASTE SATURATION PIT LAKE AT 206 METERS (675.9 FT)



Minimum Saturated Thickness Above Bottom of Waste Standard Deviation of Water Table Elevation



Saturated Thickness Above Bottom of Waste (m)

- Dry
- $0.1 0.5$  $\bullet$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0 ●
- 2.1 2.5
- > 2.5 m
- Standard Deviation of Water Table Elevation
- (m)  $\bullet$  $< 0.05$ 0.06 - 0.10  $\bullet$



0.16 - 0.20









WASTE SATURATION PIT LAKE AT 207 METERS (679.1 FT)



Minimum Saturated Thickness Above Bottom of Waste Standard Deviation of Water Table Elevation



Saturated Thickness Above Bottom of Waste (m)

- Dry
- $0.1 0.5$  $\bullet$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0 ●
- 2.1 2.5
- > 2.5 m

Standard Deviation of Water Table Elevation (m)

- $\bullet$  $< 0.05$ 0.06 - 0.10  $\bullet$ ◠
	- $0.11 0.15$ 0.16 - 0.20









Figure 6

WASTE SATURATION PIT LAKE AT 208 METERS (682.4 FT)



Minimum Saturated Thickness Above Bottom of Waste Standard Deviation of Water Table Elevation



Saturated Thickness Above Bottom of Waste (m)

- Dry
- $\bullet$  $0.1 - 0.5$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0
- 2.1 2.5
- > 2.5 m

Standard Deviation of Water Table Elevation (m)

 $< 0.05$  $\bullet$ 0.06 - 0.10  $\bullet$ 

> 0.11 - 0.15  $\bullet$ 0.16 - 0.20









WASTE SATURATION PIT LAKE AT 209 METERS (685.7 FT)





Saturated Thickness Above Bottom of Waste (m)

- Dry
- $0.1 0.5$  $\bullet$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0
- 2.1 2.5
- > 2.5 m

Standard Deviation of Water Table Elevation (m)

 $\bullet$  $< 0.05$ 0.06 - 0.10  $\bullet$ 



0.16 - 0.20

# Average Saturated Thickness Above Bottom of Waste Maximum Saturated Thickness Above Bottom of Waste









WASTE SATURATION PIT LAKE AT 210 METERS (689.0 FT)





Saturated Thickness Above Bottom of Waste (m)

- Dry
- $0.1 0.5$  $\bullet$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0 Ċ
- 2.1 2.5
- > 2.5 m

Standard Deviation of Water Table Elevation (m)

 $< 0.05$  $\bullet$ 0.06 - 0.10  $\bullet$  $0.11 - 0.15$ 













WASTE SATURATION PIT LAKE AT 211 METERS (692.3)



Minimum Saturated Thickness Above Bottom of Waste Standard Deviation of Water Table Elevation



Saturated Thickness Above Bottom of Waste (m)

- Dry
- $0.1 0.5$  $\bullet$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0 Ô
- 2.1 2.5
- > 2.5 m

Standard Deviation of Water Table Elevation (m)

 $< 0.05$  $\bullet$ 0.06 - 0.10  $\bullet$ 0.11 - 0.15

0.16 - 0.20









WASTE SATURATION PIT LAKE AT 212 METERS (695.5)



Minimum Saturated Thickness Above Bottom of Waste Standard Deviation of Water Table Elevation



Standard Deviation of Water Table Elevation

 $< 0.05$ 

0.06 - 0.10

0.11 - 0.15 0.16 - 0.20

(m)

 $\bullet$ 

 $\bullet$ 

 $\bullet$ 

Saturated Thickness Above Bottom of Waste (m)

- Dry
- $\bullet$  $0.1 - 0.5$
- $0.6 1.0$  $\bullet$
- $1.1 1.5$  $\bullet$
- 1.6 2.0  $\bullet$
- 2.1 2.5
- > 2.5 m









Figure 11

WASTE SATURATION PIT LAKE AT 213 METERS (698.8)